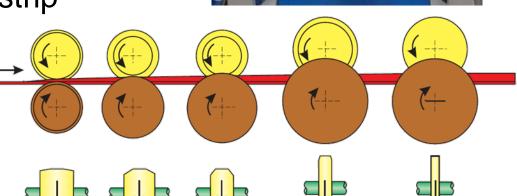
In-process Strain Measurement in Roll Forming

Florian Kern
N. Stiegler
Prof. Thomas Neitzert



Roll Forming

- Bending process
- Angle introduced continuously along straight line
- Set of contoured rolls
- Strip motion applied by rotation of rolls (friction)
- Alternatively, pulling of strip
- Unlimited length



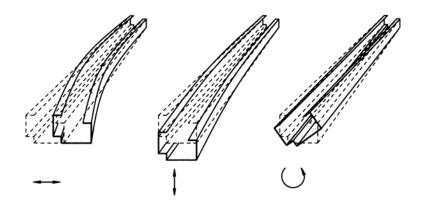


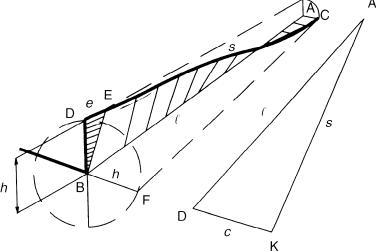
Motivation

- Geometric defects a frequent occurrence in roll forming
- Largely caused by plastic deformation outside the intended forming zone



Continuous, non-contact strain measurement in flange area



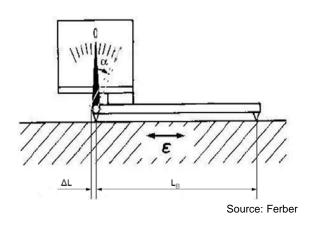


Source: Halmos

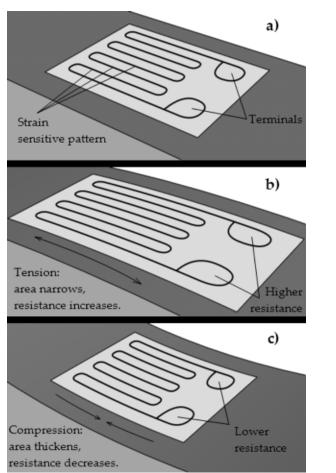


Strain Measurement Methods I

Mechanical Strain Gauge



Mechanic longitudinal strain device





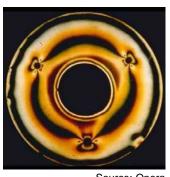


Electric conductor changes resistance when being compressed or elongated

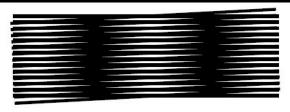
Strain Measurement Methods II

Photoelasticity





iso-chromatic and isoclinic lines in a specimen under load

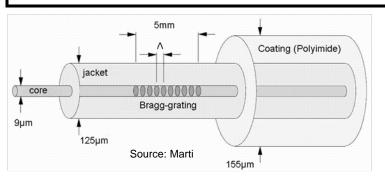


Moiré effect of two rotated superimposed line pattern

Source: Onera

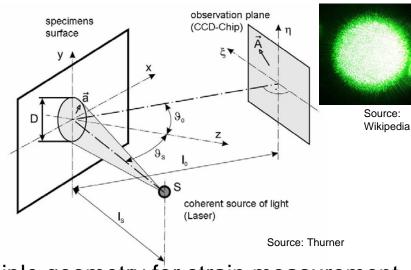
Fibre Bragg Grating

Laser Speckle



$$\Delta \varepsilon = \frac{1}{1 - p_e} \cdot \left(\frac{\Delta \lambda_B}{\lambda_B} - (\alpha - \zeta) \cdot \Delta T \right)$$



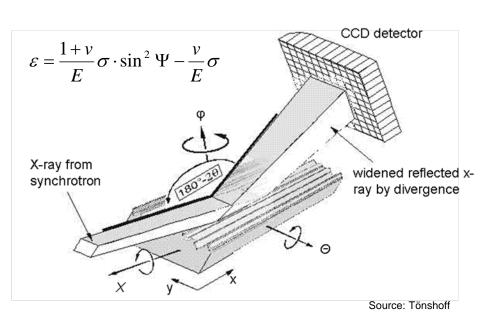


Principle geometry for strain measurement with objective Speckles

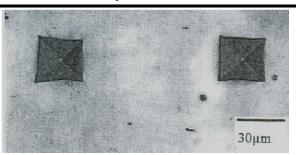
Strain Measurement Methods IV

X-ray Diffraction

Optical

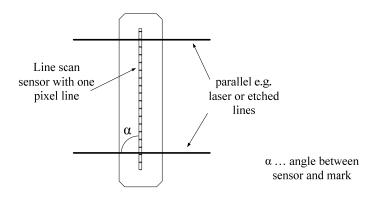


Set-up to measure strain in the surface zone of a specimen



Source: Ziebs

Vickers micro hardness indentations

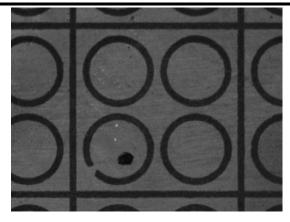


Line camera

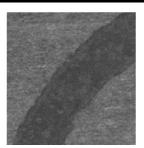


Strain Measurement Methods IV

Grid Analysis

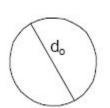


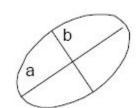




Etched (left) and laser (right) grids shown at 50x magnification, circle radius of 2.5mm

Undeformed Ø 2.5mm laser grids with straight laser lines

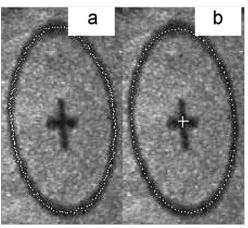




$$e_{major}(\%) = \frac{a - d_0}{d_0} \times 100$$

$$e_{\min or}(\%) = \frac{b - d_0}{d_0} \times 100$$

Deformation of a circle grid



Source: Hsu

Fitted ellipses

a: automatic grid acquisition

b: elliptic grid for a MRA



Strain Measurement - Conclusions

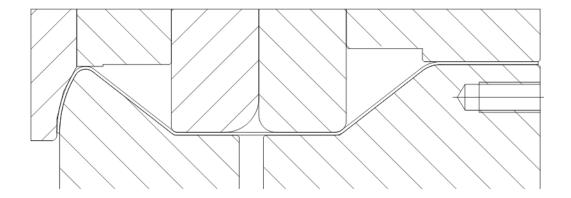
Balance between accuracy and cost

Compromise: Strain gauge

laborious preparation, but:

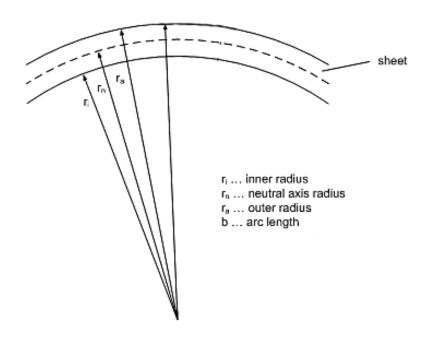
- continuous data
- •inexpensive (in comparison)
- well established
- accurate (compared to other inexpensive solutions)
- delivers full set of data (3 directions)

Problem: How to acquire bending strain with one side of the strip inaccessible?





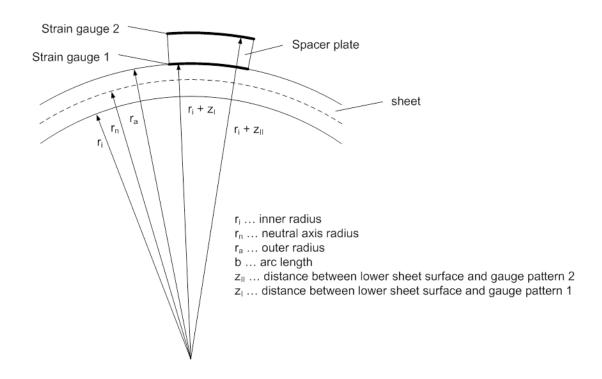
Spacer Plate – Principle I



$$\varepsilon_{O}(z) = z \left(\frac{\varepsilon_{II} - \varepsilon_{I}}{z_{II} - z_{I}} \right) + \left(\varepsilon_{I} - z_{I} \frac{\varepsilon_{II} - \varepsilon_{I}}{z_{II} - z_{I}} \right)$$

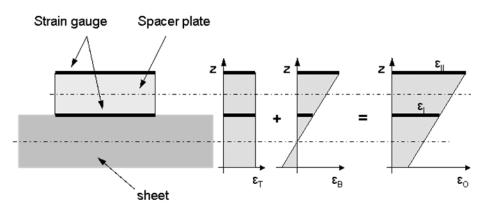


Spacer Plate – Principle I



$$\varepsilon_{O}(z) = z \left(\frac{\varepsilon_{II} - \varepsilon_{I}}{z_{II} - z_{I}} \right) + \left(\varepsilon_{I} - z_{I} \frac{\varepsilon_{II} - \varepsilon_{I}}{z_{II} - z_{I}} \right)$$

Spacer Plate – Principle II



Trend of the strain in a cross-section of sheet and spacer plate

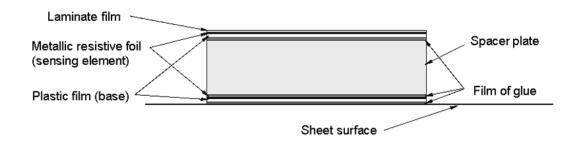
 $\epsilon_{\parallel}\dots$ strain of the gauge on the top of the spacer plate

 $\epsilon_{|}\dots$ strain of the gauge between sheet and spacer plate

 $\epsilon_{\scriptscriptstyle T} \dots$ tensile strain

 $\epsilon_{\text{B}}\dots$ bending strain

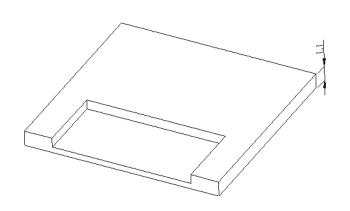
 ε_0 ... tensile + bending strain



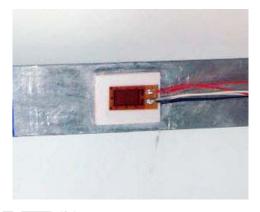
Strain measurement from one side of the sheet

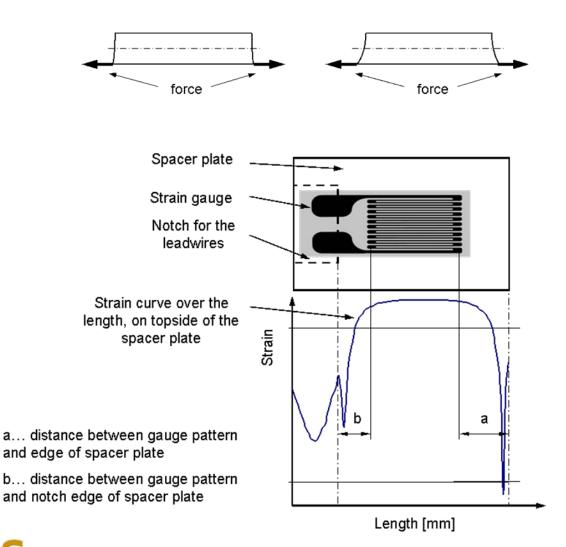


Design of Spacer Plate



ABS spacer plate





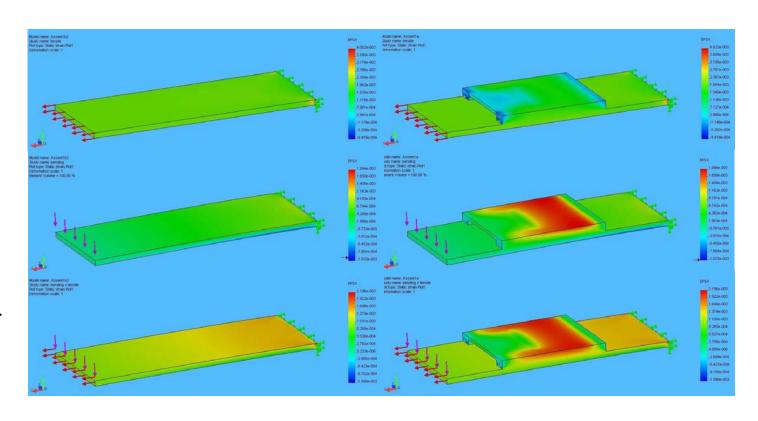


Simulation of Spacer Plate I

tensile

bending

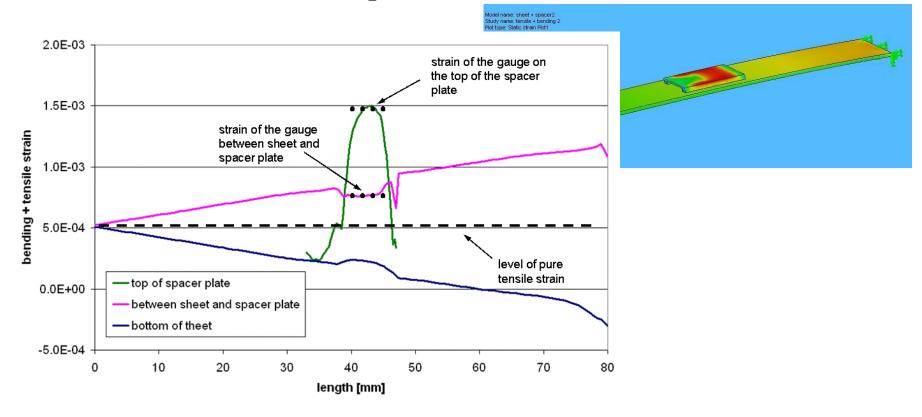
tensile + bending



Simulation of the strain layout during deformation with and without applied spacer plate on the sheet



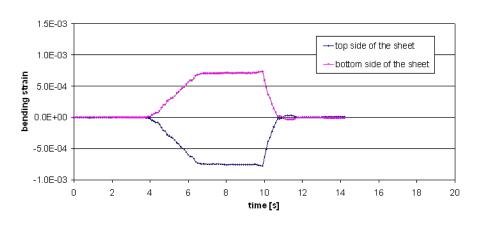
Simulation of Spacer Plate II



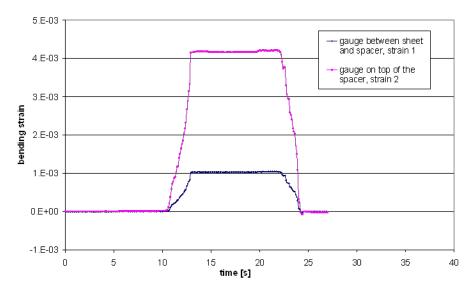
Strain in x direction (xy-plane, centre) 3.5N shear force, 1625N tensile force, 14mm long spacer plate



Accuracy of Measurement



Bending, one strain gauge on each side

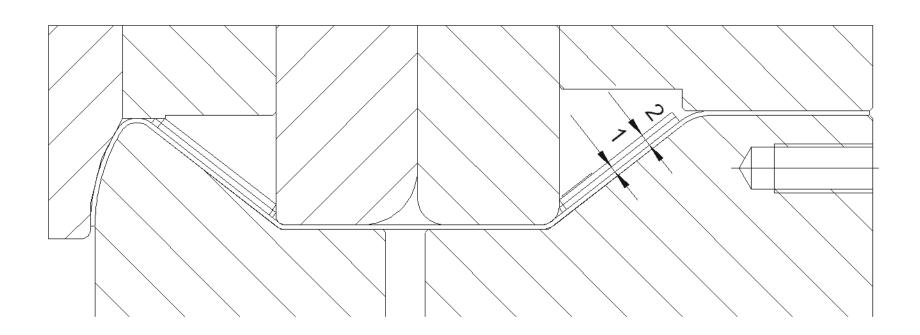


Bending, two strain gauges and spacer plate on one side of the specimen

Bending strain can be measured with accuracy of ±3%

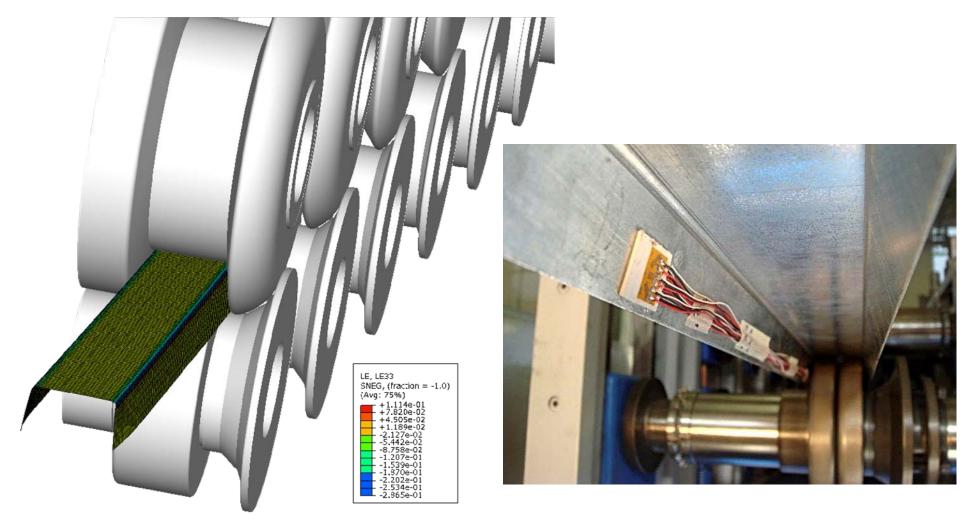


Spatial Constraints in Roll Former

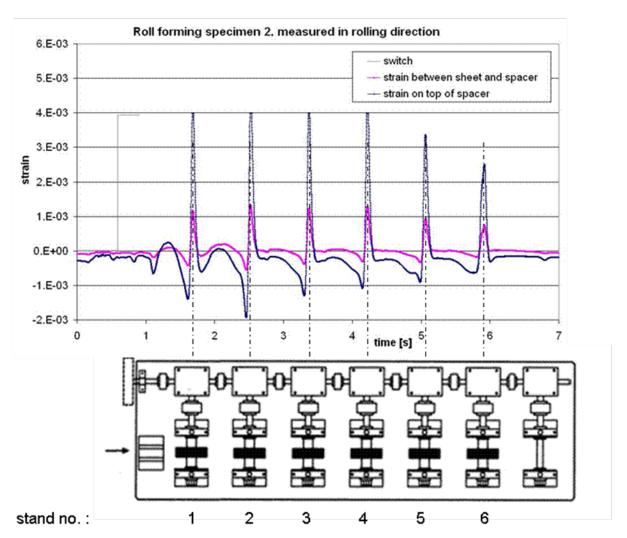




Application of strain gauge device



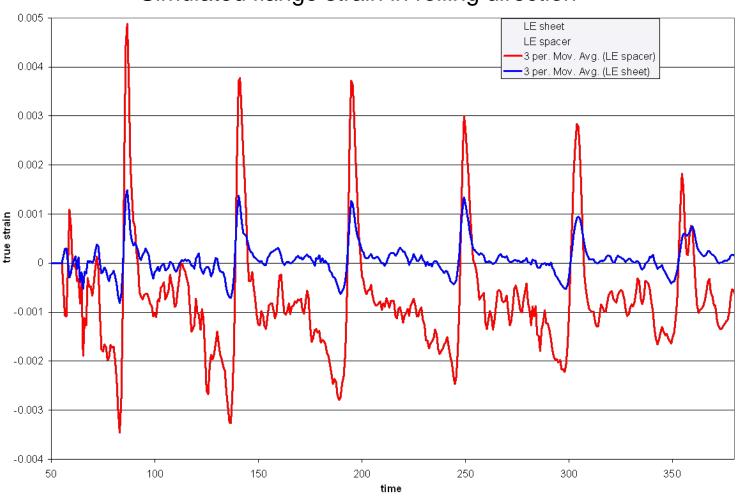
Measured Longitudinal Strain





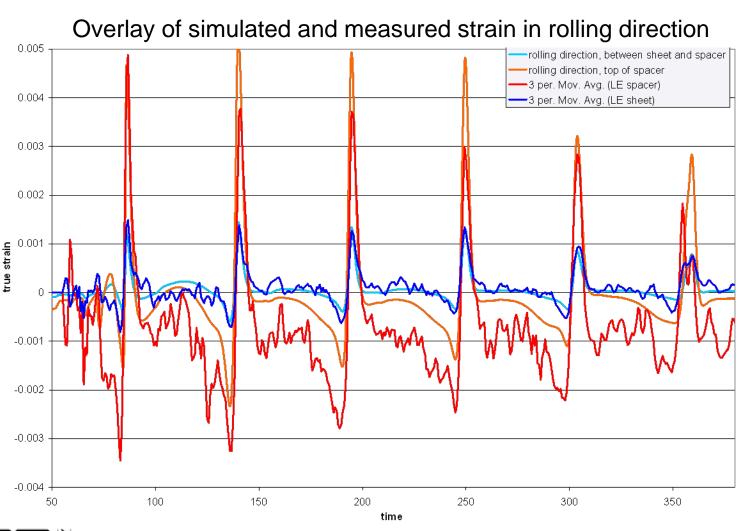
Simulated Longitudinal Strain

Simulated flange strain in rolling direction



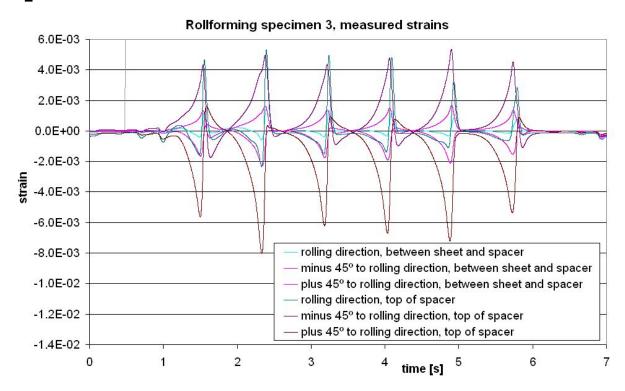


Longitudinal Strain





Principal Strain

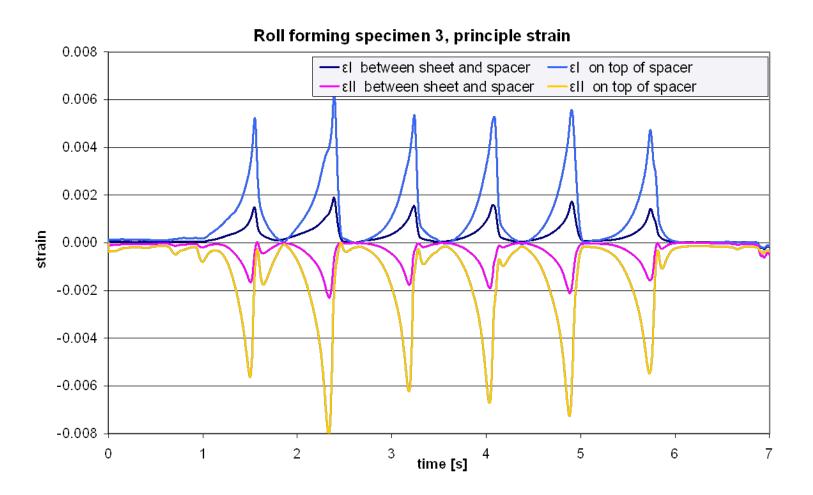


$$\varepsilon_{\text{I,II}} = \frac{\varepsilon_A + \varepsilon_C}{2} \pm \frac{1}{2} \sqrt{2} \sqrt{\left(\varepsilon_A - \varepsilon_B\right)^2 + \left(\varepsilon_B - \varepsilon_C\right)^2}$$

$$\tan 2\phi = \frac{\varepsilon_A - 2\varepsilon_B + \varepsilon_C}{\varepsilon_A - \varepsilon_C}$$

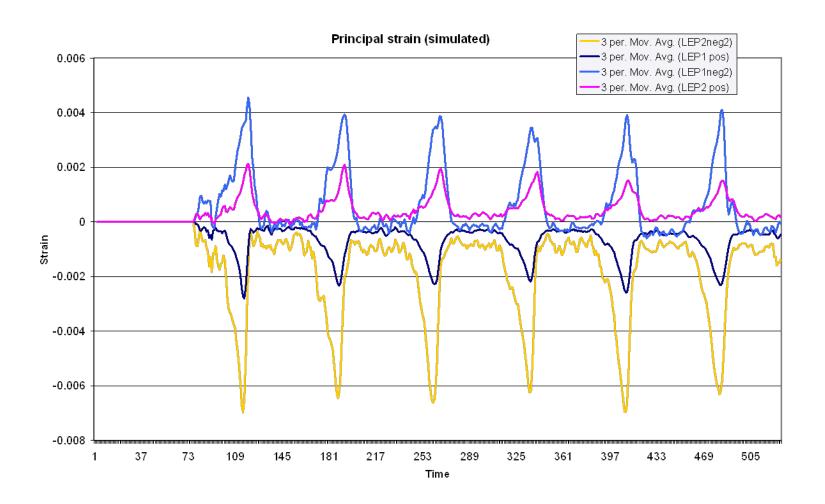


Principal Strain - Measured





Principal Strain - Simulated





Summary and future work

- Review of strain measurement methods
- Design of strain gauge device that acquires all desired data from one side of the strip
- Agreement between measurements and simulation

Gather data under conditions that generate geometric

deviations

 Develop rules for corrective intervention



